

Application of

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**CATHETER SHAFT JUNCTION HAVING A POLYMERIC REINFORCING  
MEMBER WITH A HIGH GLASS TRANSITION TEMPERATURE**

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# CATHETER SHAFT JUNCTION HAVING A POLYMERIC REINFORCING MEMBER WITH A HIGH GLASS TRANSITION TEMPERATURE

## BACKGROUND OF THE INVENTION

This invention relates generally to catheters, and particularly to intravascular catheters for use in percutaneous transluminal coronary angioplasty (PTCA), or the delivery of stents.

5 In a typical PTCA procedure, a dilatation balloon catheter is advanced over a guidewire to a desired location within the patient's coronary anatomy to position the balloon of the dilatation catheter along the stenosis to be dilated. The balloon is then inflated one or more times with fluid at relatively high pressures (generally 4-16 atmospheres) to dilate the stenosed region of the  
10 diseased artery. A stent is commonly implanted within the artery, typically by delivery to the desired location within the artery in a contracted condition on a balloon of a catheter which is similar in many respects to a balloon angioplasty catheter. Inflation of the balloon expands the stent, thereby implanting it in the artery. Following the dilatation or stent expansion, the balloon is deflated and  
15 the catheter repositioned or withdrawn from the artery.

In rapid exchange type balloon catheters, the catheter has an inflation lumen extending from the proximal end of the catheter to a balloon on a distal shaft section, a distal guidewire port at the distal end of the catheter, a proximal guidewire port located distal to the proximal end of the catheter, and  
20 a relatively short guidewire lumen extending therebetween. The rapid

exchange junction located at the proximal guidewire port should provide a good transition in flexibility from the relatively stiff proximal shaft section to the relatively flexible distal shaft section. One difficulty has been forming a junction which is flexible, yet kink resistant and rugged.

5 To help meet the desire for a catheter having sufficient pushability and crossability, while maintaining trackability within the patient's tortuous vasculature, prior art designs have supplemented polymer catheter shafts with a support mandrel. Other prior art designs have addressed these handling and performance issues by using materials of different stiffness for the  
10 proximal and distal portions of the catheter, and employing a high strength metallic proximal shaft section, commonly called a hypotube. To prevent kinking at the junction of these two materials, while maintaining trackability, some conventional designs have employed reinforcing layers or stiffening wires to bridge the transition in catheter shaft material. Despite these  
15 attempts, prior art designs have suffered from various drawbacks relating to these handling and performance issues.

Accordingly, it would be a significant advance to provide a catheter having an improved catheter shaft junction between shaft sections such as the proximal and distal shaft sections. This invention satisfies these and other  
20 needs.

## **SUMMARY OF THE INVENTION**

The invention is generally directed to a catheter, and preferably a balloon catheter, having a polymeric reinforcing member at a junction between shaft sections such as the junction between the proximal shaft section and the distal shaft section. In a presently preferred embodiment, the balloon catheter is a rapid exchange type catheter. The polymeric reinforcing member is around or within either or both of the tubular member defining the inflation lumen or the tubular member defining the guidewire lumen at the rapid exchange junction. The reinforcing tubular member at the rapid exchange junction of the shaft prevents or inhibits damage to the tubular members defining the inflation lumen and/or guidewire lumen during assembly or use of the catheter, and thus avoids a loss of lumen integrity.

The catheter of the invention generally comprises an elongated shaft having a proximal shaft section, a distal shaft section, a first lumen (e.g., an inflation lumen), a second lumen (e.g., a guidewire receiving lumen) extending within at least the distal shaft section. A balloon catheter of the invention has a balloon on the distal shaft section with an interior in fluid communication with the inflation lumen. The shaft proximal shaft section comprises a proximal tubular member having a proximal end, a distal end, a distal portion, and defining a proximal portion of the inflation lumen. The shaft distal shaft section comprises an outer tubular member and an inner tubular member within the outer tubular member lumen. The outer tubular member defines a distal

portion of the inflation lumen, and the inner tubular member defines the guidewire receiving lumen in fluid communication with a guidewire distal port at the distal end of the catheter shaft, and a guidewire proximal port at the proximal end of the inner tubular member. As a rapid exchange type catheter,

5 the proximal guidewire port at the rapid exchange junction is located at the proximal end of the distal shaft section, distal to the proximal end of the catheter shaft. The inner tubular member has a proximal portion generally in a side-by-side relationship with the distal portion of the proximal tubular member. The polymeric reinforcing member is located around or within the

10 proximal portion of the inner tubular member or the distal portion of the proximal tubular member.

The polymeric reinforcing member is preferably a tube having a shape configured to correspond to the shape of the proximal portion of the inner tubular member or the distal portion of the proximal tubular member, such as a

15 circular, oblong/oval, D-shaped or C-shaped transverse cross section. However, a variety of suitable shapes may be used depending on the shape of the inner tubular member and the proximal tubular member. In a presently preferred embodiment, the polymeric reinforcing member is formed of a first polymeric material having a glass transition temperature greater than a glass

20 transition temperature of a second polymeric material forming the distal portion of the proximal tubular member or the proximal portion of the inner tubular member. The first polymeric material forming the polymeric reinforcing

member is preferably a high temperature, high modulus material, having a glass transition temperature ( $T_g$ ) of about 300°C to about 450°C, and a tensile modulus, expressed as a secant modulus (ASTM D882) of about 350,000 to about 450,000 psi. In one embodiment, the first polymeric material forming the polymeric reinforcing member is selected from the group consisting of thermoset polyimide and thermoplastic polyimide. The thermoset or thermoplastic polyimide has a high secant modulus of greater than about 350,000 psi, with about 25,000 to about 30,000 psi tensile strength, which allows for a thin-walled reinforcing tube which nonetheless has a sufficient strength to provide the required reinforcement. In a presently preferred embodiment, thermoset polyimide is used, due to the high glass transition temperature of the thermoset polyimide. The thermoset polyimide has a very high glass transition temperature ( $T_g$ ) of approximately 400 °C (as measured by differential scanning calorimetry (DSC)), and thus excellent dimensional stability at the processing temperature of other polymers such as polyamides and polyurethanes commonly used in catheter components. As a result, the polyimide tube maintains thin-walled, controlled dimensions during formation and assembly of the catheter, and specifically during high temperature fusion (i.e., thermal) bonding of the tubular members to form the rapid exchange junction. Thermoplastic polyimide, which has a  $T_g$  of about 250°C, may also be used, but is less preferred than the high glass transition temperature thermoset polyimide.

In one embodiment, the second polymeric material forming the distal portion of the proximal tubular member or the proximal portion of the inner tubular member is selected from the group consisting of polyether block amide (PEBAX), nylon, and polyurethane, although a variety of suitable polymeric materials different from the first polymeric material and useful in the formation of catheter shafts can be used. The glass transition temperature of the second polymeric material forming the distal portion of the proximal tubular member or the proximal portion of the inner tubular member is typically about 30°C to about 60°C, and more specifically about 35°C to about 55°C.

Similarly, in one embodiment, the polymeric material forming a proximal portion of the outer tubular member is selected from the group consisting of PEBAX, nylon, and polyurethane, although a variety of suitable polymeric materials different from the first polymeric material and useful in the formation of catheter shafts can be used. The distal portion of the proximal tubular member and the proximal portion of the inner tubular member are preferably formed of compatible materials which are fusion bondable together. In one embodiment, adhesive is not used at the rapid exchange junction to bond the distal portion of the proximal tubular member and the proximal portion of the inner tubular member together, which are instead fusion bonded together.

The polymeric reinforcing member has sufficient wall thickness to prevent or inhibit the formation of a break in the wall of the tubular members defining the inflation lumen and the guidewire lumen at the rapid exchange

junction. During assembly of the catheter, assembly mandrels or rods (hereafter "assembly rods"), are placed in the lumens of the proximal tubular member and the distal inner tubular member, to keep the lumens open during fusion of the tubular members to form the rapid exchange junction. Heat, and pressure from shrink tubing are applied to the tubular members to fusion bond the tubular members together and form the rapid exchange junction at the transition between the proximal or an intermediate shaft section and the distal shaft section at the guidewire proximal port. The polymeric reinforcing member prevents or inhibits loss of integrity of the inner tubular member and proximal tubular member caused by junction formation as the heated polymeric material of the tubular members are flow together during fusion bonding. Thus, leaks in the guidewire and inflation lumens are prevented or inhibited by the polymeric reinforcing member with a high glass transition temperature.

In one embodiment, a supporting member such as a mandrel is provided within at least a section of the inflation lumen, to enhance the catheter's pushability and crossability. The length and position of the support mandrel within the catheter shaft may vary. Typically, the support mandrel extends distally from the proximal end of the catheter shaft, or from an intermediate location distal to the proximal end of the catheter shaft,. The support mandrel is preferably a solid metal or high modulus polymer material, although a variety of different supporting members can be used including solid



or hollow rods, wires, and the like. In the embodiment having the polymeric reinforcing member in the inflation lumen, the support mandrel extends adjacent an inner or outer surface of the polymeric reinforcing member, either in contact with or spaced apart from the surface of the polymeric reinforcing member. In one embodiment the support mandrel is releasably secured (i.e., not fixedly secured) to the shaft, and is thus free to be removed therefrom. In an alternative embodiment, the support mandrel distal section is embedded in polymeric material at or near the rapid exchange junction. The polymeric reinforcing member prevents or inhibits the support mandrel from extending through, and causing a leak in, the tubular members at the rapid exchange junction. In one embodiment, the support mandrel is bonded to the polymeric reinforcing member. In one embodiment, to facilitate bonding the support mandrel to the polymeric reinforcing member, the polymeric reinforcing member is a multilayered tube having a first layer formed of the first polymeric material (e.g., polyimide), and at least a second layer which is an inner or an outer layer and which is formed of a different polymeric material, such as PEBAX, nylon, polyurethane or polyolefin hot melt adhesive such as Primacor (an EAA copolymer), which adheres to metal.

The balloon catheter of the invention can be configured for a variety of applications including coronary angioplasty, peripheral dilatation, stent or graft delivery, drug delivery, and the like. A variety of suitable stents can be used with the balloon catheter of invention, which generally comprise expandable

tubular members (for details of stent design, see for example US Patent Nos. 5,507,768 (Lau et al.) and 5,458,615 (Klemm et al.), incorporated by reference herein in their entireties).

The catheter of the invention maintains the integrity of the inflation lumen and guidewire lumen throughout assembly and use of the catheter, due to the polymeric reinforcing member. The thin-walled polymeric reinforcing member has excellent dimension stability providing a rapid exchange junction having a low profile and a suitable stiffness transition between proximal and distal portions of the catheter, to thereby improve handling and performance and minimize kinking. These and other advantages of the invention will become more apparent from the following detailed description and exemplary drawings.

### **BRIEF DESCRIPTION OF THE DRAWINGS**

Fig. 1 is an elevational view, partially in section, of a rapid exchange balloon catheter which embodies features of the invention, having a polymeric reinforcing tube in the inflation lumen in the distal end of the proximal tubular member, with a support mandrel having a distal section extending along an inner surface of the polymeric reinforcing tube.

Fig. 2 is a transverse cross sectional view of the catheter shown in Fig. 1, taken along lines 2-2.

Fig. 3 is a transverse cross sectional view of the catheter shown in Fig. 1, taken along lines 3-3.

Fig. 4 is longitudinal cross section of an alternative rapid exchange junction which embodies features of the invention, prior to fusing of the tubular members together to form the junction during catheter assembly, having a polymeric reinforcing tube in the inflation lumen in the distal end of the proximal tubular member, with a support mandrel having a distal section extending along an outer surface of the polymeric reinforcing tube.

Fig. 5 is a longitudinal cross section of the rapid exchange junction shown in Fig. 4, after fusing of the tubular members together to form the junction.

Fig. 6 is a transverse cross sectional view of the catheter shown in Fig. 5, taken along lines 6-6.

Fig. 7 is a transverse cross sectional view of the catheter shown in Fig. 5, taken along lines 7-7.

Fig. 8 is longitudinal cross section of an alternative rapid exchange junction which embodies features of the invention, having the polymeric reinforcing tube on an outer surface of the proximal portion of the inner tubular member, with a support mandrel in the inflation lumen in the proximal tubular member.

Fig. 9 is a transverse cross sectional view of the catheter shown in Fig. 8, taken along lines 9-9.

Fig. 10 is a transverse cross sectional view of the catheter shown in Fig. 8, taken along lines 10-10.

Fig. 11 is longitudinal cross section of an alternative rapid exchange junction which embodies features of the invention, having the polymeric reinforcing tube on an inner surface of the proximal portion of the inner tubular member, with a support mandrel in the inflation lumen in the proximal tubular member.

Fig. 12 is a transverse cross sectional view of the catheter shown in Fig. 11, taken along lines 12-12.

Fig. 13 is a transverse cross sectional view of the catheter shown in Fig. 11, taken along lines 13-13.

### **DETAILED DESCRIPTION OF THE INVENTION**

Fig. 1 illustrates rapid exchange type balloon catheter 10 embodying features of the invention. Catheter 10 generally comprises an elongated catheter shaft 11 having a proximal end 12, a distal end 13, a proximal shaft section 18 and a distal shaft section 19 at the distal end of the proximal shaft section, and an inflatable balloon 14 on the distal shaft section. The shaft 11 has an inflation lumen 20, and a guidewire receiving lumen 21. The proximal shaft section 18 comprises a proximal tubular member 22 defining a proximal portion of the inflation lumen 20, and having a proximal end 23, a distal end 24, and a distal portion 25. In the embodiment illustrated in Fig. 1, the distal end of the proximal tubular member 22 tapers distally to a smaller transverse dimension. The distal shaft section 19 comprises an outer tubular member 26 defining a distal portion of the inflation lumen 20, and an inner tubular member

27 defining the guidewire lumen 21 in fluid communication with a guidewire distal port 28 at the distal end of the catheter and a guidewire proximal port 29 at the proximal end of the inner tubular member 27, configured to slidably receive guidewire 40 therein. A rapid exchange junction at the guidewire proximal port 29 is the transition between the single lumen proximal shaft section and the multilumen distal shaft section. As best illustrated in Figs. 2 and 3, showing transverse cross sections of the catheter of Fig. 1, taken along lines 2-2 and 3-3, respectively, the outer tubular member 26 is around and joined to both the inner tubular member 27 and the proximal tubular member 22. Balloon 14 has a proximal end sealingly secured to the distal end of outer tubular member 26 and a distal end sealingly secured to the distal end of inner tubular member 27, so that its interior is in fluid communication with inflation lumen 20. An adapter 41 at the proximal end of the catheter provides access to the inflation lumen 20. The distal end of catheter may be advanced to a desired region of a patient's body lumen in a conventional manner and balloon 14 inflated to perform a procedure such a dilate a stenosis, and catheter withdrawn or repositioned for another procedure.

In the embodiment of Fig. 1, the inner tubular member 27 has a proximal portion 31 in a side-by-side relationship with the distal portion 25 of the proximal tubular member 22. The inner tubular member 27 is joined to an inner surface of the outer tubular member 26 and to an outer surface of the proximal tubular member 22. Distal to the side-by-side portions 25, 31, the



rod (not shown), and positioned within the distal end section of the proximal tubular member 22. It should be understood that the proximal tubular member 22 may be a single tubular member, or alternatively multiple tubes joined end to end, so that the polymeric reinforcing member 32 is positioned within a  
5 distal tube of the proximal tubular member 22. For example, in the embodiment in which the proximal portion of the proximal tubular member 22 is formed of a polyetherether ketone (PEEK) tubular member or a metal hypotube, a distal tube such as a polyether block amide (PEBAX) or nylon tubular member is typically bonded to the distal end of the PEEK or hypotube  
10 tubular member, and the polymeric reinforcing member 32 placed within the PEBAX or nylon tubular member. The thus combined assembly rod, polymeric reinforcing member 32, and proximal tubular member 22 are then placed in part within the outer tubular member 26 and aligned with the inner tubular member 27, to be radially adjacent to the guidewire proximal port 29  
15 area. An assembly rod (not shown) is positioned in the inner tubular member 27, and the thus assembled rapid exchange junction heated with shrink tubing (not shown) therearound to shrink the shrink tubing and form the thermally fused junction. The shrink tubing and assembly rods are removed, and a reinforcing mandrel 36 is inserted. Due to the high glass transition  
20 temperature of the polymeric reinforcing member 32, the integrity of the inflation lumen 20 is maintained. The polymeric reinforcing member 32 of Fig. 1 typically has a length of about 2 to about 10 cm, preferably about 5 cm, an

outer diameter of about 0.46 to about 0.83 mm, an inner diameter of about 0.45 to about 0.8 mm, and a wall thickness of about 0.01 to about 0.03 mm.

The polymeric reinforcing member 32 is formed of a first polymeric material having a glass transition temperature greater than a glass transition temperature of a second polymeric material forming the distal portion of the proximal tubular member 22 or the proximal portion of the inner tubular member 27. In a presently preferred embodiment, the second polymeric material forming the distal portion of the proximal tubular member 22 or the proximal portion of the inner tubular member 27 is nylon or a copolyamide such as PEBAX. In a presently preferred embodiment, the first polymeric material is thermoset polyimide. A polyimide reinforcing member 32 is typically formed by a solution process, such as by dip coating a mandrel and removing the mandrel, to thereby produce a tubular member. In a suitable solution forming process, a polyimide solution is dip, or otherwise, coated onto a neckable mandrel, as described in U.S. Patent Nos. 4,826,706 and 4,659,622, and the Manufacturing Process section of the Phelps Dodge High Performance Conductors brochure, A Primer on Polyimide Tubing, pp. 1, incorporated herein by reference in their entireties, and then separated intact from the mandrel, to thereby produce a tubular member. The dip coated mandrel can be passed through dies to control the outer dimension of the polyimide reinforcing member 32, and the diameter of the removable mandrel determines the inner diameter of the polyimide reinforcing member 32.



In a presently preferred embodiment, the polymeric reinforcing member 32 is a solid-walled tube. In one embodiment, the polymeric reinforcing member 32 consists of a polyimide tube. However, in alternative embodiments, the polymeric reinforcing member 32 is a multilayered tube having a first inner or outer layer formed of the first polymeric material (e.g., polyimide), and a second layer on a surface of the first layer, the second layer being formed of a third polymeric material (not shown). In a presently preferred embodiment, the third polymeric material is the same polymer family as, and compatible with, the second polymeric material forming the distal end of the proximal tubular member 22. The third polymeric material is typically a polyamide such as nylon or PEBAX, or an adhesive polymer such as the ethylene based adhesive PRIMACOR, providing improved bonding of the polymeric reinforcing member 32 to the proximal tubular member 22, or to the inner tubular member 27 (see embodiments of Figs. 8 and 11). Although illustrated as a single layer in Fig. 1, the inner tubular member 27 may alternatively comprise a multilayered tubular member, which in one embodiment has an outer layer formed of the second polymeric material (e.g., nylon or PEBAX).

Support mandrel 36 within the inflation lumen 20 extends from the proximal end 12 of the catheter shaft 11 to the distal end 24 of the proximal tubular member 22 in the embodiment of Fig. 1. The support mandrel 36 is formed of a material selected from the group consisting of metals such as



Figs. 4 and 5 illustrate an alternative rapid exchange junction embodying features of the invention, in which the support mandrel 36 extends within the proximal tubular member 22 and adjacent to the outer surface of the polymeric reinforcing member 32 in the proximal tubular member 22. As best  
5 illustrated in Figs. 6 and 7, showing transverse cross sectional views of the catheter of Fig. 5, taken along lines 6-6 and 7-7, respectively, the support mandrel extends in the proximal tubular member 22 from the proximal end to the distal end thereof. Fig. 4 illustrates the rapid exchange junction of Fig. 5, before the tubular members 22, 26 and 27 are fused together during catheter  
10 assembly. The catheter of Fig. 5 is assembled as outlined above for the embodiment of Fig. 1, except that an outer surface of the polymeric reinforcing member 32 is first bonded to an outer surface of the support mandrel 36 by adhesive bonding, or by fusion bonding to an outer bondable layer of the polymeric reinforcing member 32. Assembly rods (not shown) are placed  
15 within the lumens of the inner tubular member 27 and the proximal tubular member 22/polymeric reinforcing member 32 to keep the lumens open during the application of heat and pressure to fuse the tubular members 22, 26 and 27 together. The proximal tubular member 22 is then positioned around the support mandrel 36/polymeric reinforcing member 32 assembly, and, with an  
20 inflation lumen shaping assembly rod positioned in the polymeric reinforcing member and an assembly rod in the inner tubular member, shrink tubing

around the outer tubular member 26 is heated to fuse the tubular members 22, 26 and 27 together and form the rapid exchange junction illustrated in Fig. 5.

Fig. 8 illustrates an alternative rapid exchange junction embodying features of the invention, in which the polymeric reinforcing member 32 is on an outer surface of the proximal portion 31 of the inner tubular member 27. Support mandrel 36 extends within the proximal tubular member 22 from the proximal end to the distal end thereof. Figs. 9 and 10 illustrate transverse cross sectional views of the catheter of Fig. 8, taken along lines 9-9, and 10-10, respectively. As best illustrated in Fig. 10, the distal end of the inflation lumen defined by the distal portion 25 of the proximal tubular member 22 is D-shaped. The D-shaped lumen section results from the shape of the assembly rod positioned in the proximal tubular member 22 during fusion of the tubular members. In alternative embodiments, the inflation lumen 20 may have a circular or oval shape. In the embodiment of Fig. 8, the polymeric reinforcing member 32 has a length approximately equal to the length of the proximal portion 31 of the inner tubular member 27 which is in a side-by-side relationship with the distal portion of the proximal tubular member 22. Alternatively, the distal end of the polymeric reinforcing member 32 may be located distal to the distal end of the proximal portion 31 of the inner tubular member 27. Polymeric material or filler 42 (see Fig. 10) typically fills the space within the outer tubular member 26 at the rapid exchange junction,

between the outer tubular member 26 and the inner tubular member 27/proximal tubular member 22.

Fig. 11 illustrates an alternative rapid exchange junction embodying features of the invention, in which the polymeric reinforcing member 32 is on an inner surface of the proximal portion 31 of the inner tubular member 27. Support mandrel 36 extends within the proximal tubular member 22 from the proximal end to the distal end thereof. Figs. 12 and 13 illustrate transverse cross sectional views of the catheter of Fig. 11, taken along lines 12-12, and 13-13, respectively.

In the illustrated embodiments, the proximal tubular member 22 is a single tubular member. In an alternative embodiment (not shown), the proximal tubular member 22 comprises a first tube, and a second tube distal to the first tube and having a proximal end bonded to a distal end of a first tube and forming the distal portion of the proximal tubular member 22. Thus, the proximal tubular member second tube forms a midshaft section, between the proximal first tube and the distal shaft section. The proximal tubular member first tube is typically formed of a material selected from the group consisting of a metal such as stainless steel, and a high modulus polymer such as PEEK or nylon, and in a presently preferred embodiment, the second tube is formed at least in part of the second polymeric material (e.g., nylon or PEBAX), typically adhesively bonded to the first tube.

The proximal tubular member 22, inner tubular member 27, and outer tubular member 26 of the catheters of the invention may be formed by conventional techniques, e.g. extruding, from materials already found useful in intravascular catheters such as polyethylene, polyamide, polyesters and composite materials. The use of the support mandrel 36 allows the use of otherwise soft materials, such as polyamide block copolymers, co-polyesters, nylon and polyurethanes, which are compatible with materials used to form dilatation balloons. This facilitates the bonding of the outer 26 and inner 27 tubular members to the balloon 14 by conventional techniques, such as laser bonding. The catheter components can be bonded together by heat fusion, adhesive, or by other conventional means. The polymeric reinforcing member 32 may be adhesively bonded, fusion bonded, or friction fit around or within the inner tubular member or the proximal tubular member, and is preferably secured thereto by ultraviolet curing adhesive such as is available from Loctite Corporation.

The catheter shaft will generally have the dimensions of conventional dilatation or stent delivery catheters. The length of the catheter 10, measured from the distal end of the adapter 30 to the distal end of the catheter is about 90 to about 150 cm, typically about 137 cm. The proximal tubular member 22 of the proximal shaft section 18 has a length of about 110 to about 120 cm, typically about 114 cm, an outer diameter (OD) of about 0.6 to about 1.3 mm, and an inner diameter (ID) of about 0.5 to about 1.1 mm. The outer tubular

member 26 of the distal shaft section 19 has a length of about 25 to about 35 cm, typically about 27 cm, an OD of about 0.76 to about 1.3 mm, and an ID of about 0.71 to about 1.2 mm. The inner tubular member 27 of the distal shaft section 19 has a length of about 25 to about 35 cm, typically about 29 cm, an  
5 OD of about 0.5 to about 0.63 mm, and an ID of about 0.38 to about 0.5 mm. The inner and outer tubular members 27/26 may taper in the distal section to a smaller OD or ID. The diameter of support mandrel 36 may be adjusted as desired to achieve the desired handling characteristics, but generally should be about 0.005 to about 0.015 inch. The support mandrel 36 length is  
10 generally about 110 to about 125 cm.

The balloon 14 may be formed of a variety of suitable compliant, semi- or non-compliant, or hybrid compliant materials depending on the use of the catheter, e.g., dilatation, stent delivery, etc. The length of the balloon 14 is typically about 10 to 50 mm, more specifically about 18 to 40 mm. In an  
15 expanded state, the balloon diameter is typically about 1.5 to about 5 mm, more specifically about 1.5 to about 4 mm. The wall thickness will vary depending on the burst pressure requirements and hoop strength of the balloon material.

While the present invention is described herein in terms of certain  
20 preferred embodiments, those skilled in the art will recognize that various modifications and improvements may be made to the invention without departing from the scope thereof. Moreover, although individual features of

one embodiment of the invention may be discussed herein or shown in the drawings of the one embodiment and not in other embodiments, it should be apparent that individual features of one embodiment may be combined with one or more features of another embodiment or features from a plurality of embodiments.